

An analytical representation of airfoils

Valentin Ioan Remus NICULESCU^{*,1}, Mihnea BUTIURCA², Dumitru POPESCU³,
Stefan STEBLEA⁴

*Corresponding author

¹National Institute for Laser and Radiation physics, Bucharest,
filo_niculescu@yahoo.com

²University of Cambridge, United Kingdom,
mb2619@cam.ac.uk

³Department of Mathematical Modeling in Life Sciences,
“Gheorghe Mihoc-Caius Iacob” Institute for Mathematical, Statistical and Applied
Mathematics of the Romanian Academy,
dghpopescu@gmail.com

⁴“Ion Mincu” National University of Urban and Architecture,
stefansteblea@gmail.com

DOI: 10.13111/2066-8201.2025.17.4.9

Received: 24 October 2025/ Accepted: 16 November 2025/ Published: December 2025

Copyright © 2025. Published by INCAS. This is an “open access” article under the CC BY-NC-ND
license (<http://creativecommons.org/licenses/by-nc-nd/4.0/>)

Abstract: An important part of the construction of an aircraft is the shape of the wings. Their aerodynamics involve numerous evaluations and simulations through fluid dynamics. The reduction of the evaluation times is achieved by a parametric function. This is represented by the ratio of two polynomials. This representation will be important in order to reduce computation time for artificial network applications. The number of parameters is reduced. The analytical shape of the wing section implies analytical expression for wing parameters: maximum thickness, maximum camber, maximum camber position, minimum thickness position, and so on. These characteristics have algebraic expressions that involve arithmetic operations. We have constructed a simple mathematical wing model. We replace the discrete wing shape with a continuous form, which is described by lacunary polynomials.

Key Words: Wing geometric characteristics, lacunary polynomials, lift force, drag force

1. INTRODUCTION

In this work, we present a method for airfoil parametrization using a function of the following form:

$$f(x) = \frac{\sum_{i=0}^{i=n_1} a_i x^i}{\sum_{i=0}^{i=n_2} a_i x^i}$$

We analyze the effectiveness of our method on airfoil parametrization and compare it with Class Shape Transformation (CST) [1]. We conclude that our method is comparable to CST in terms of number of parameters used and precision, but it has an advantage on heavily cambered airfoils, where CST might struggle to achieve high levels of precision.

Multi-objective optimization problems are a common occurrence in all fields of modern science and engineering, and aircraft design is no different. The shape of the aircraft wing is almost always complex, non-linear, and highly optimized for specific conditions, and computer simulations of fluid flows are a fundamental step in the process.

Aircraft wing sections are shaped like airfoils, so as to maximize lift and minimize drag. These airfoils often need to be parametrized, meaning having an analytical shape ascribed to them, in order to be properly optimized.

Niculescu et. al. [2] first came up with the idea of using a ratio of 2 polynomials in order to parametrize airfoils, using a formula of the following form:

$$f(x) = \frac{gx}{x^2 + h^2}$$

In this work we expand upon his idea, by using higher degree polynomials for both the numerator and the denominator, up to the 6th degree, and we will analyze its performance against other well-known parametrization methods.

2. THEORETICAL METHOD

We start with a given airfoil from publicly available databases [3], and take its coordinates at different points. The points are then divided into an upper surface, and a lower surface.

Each surface is analyzed separately. The data is then fitted with a function of our form, for different degrees for both numerator and denominator (2/4, 3/4, 6/4, etc.), as well as CST using Bernstein basis. Note that for the CST fit, since it would be a non-linear system, we have used an evolutionary algorithm (CMA-ES [5], [6], with population size 128 and 3000 iterations) to get the best solution available (the lowest RMS error). Note that for the CST fit, we have used 11 polynomial indices, as well as variable N1 and N2. We have also introduced a trailing edge thickness and chord angle for the relevant airfoils.

For the rational fit, we obtain it in 2 ways: first, through the same CMA-ES algorithm as for the CST, and second, through the `curve_fit` function available in python. That way, we hope to circumvent the limitations of our stochastic algorithm, and see how good our fit would be for an optimized version of the algorithm.

Two metrics are used to evaluate our method: the max. error as a % of chord, and the max. error as a % of chord.

A fit is considered acceptable if it satisfies the following 2 criteria:

1. max.error as a % of chord < 0.25% (most CFD simulations only go up to a similar accuracy)
2. average. error as a % of chord < 0.15%

After both fits are calculated we then compare them on accuracy (if both are acceptable) and number of parameters used.

The less parameters used, the better. Thus if our fit uses less parameters than the other methods, with a similar or better precision, then our fit is better.

We have analyzed 50 different airfoils, from a different range of engineering applications [7]. We chose the lower surface and chose a rational fit with the numerator a 6th degree polynomial, and a 4th degree polynomial as the denominator.

3. RESULTS

We then tabulated the data for both the maximum error and the root-mean-square error.

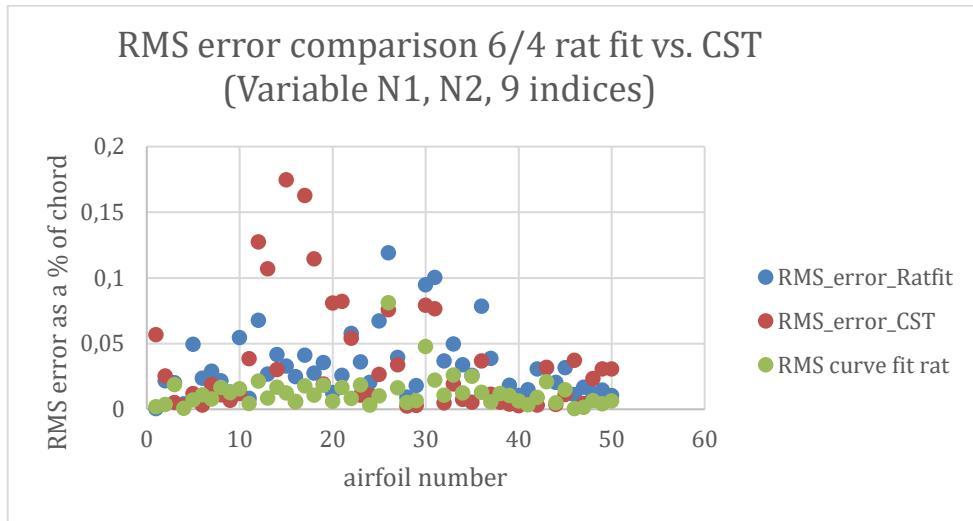


Fig 1. RMS error comparison for Rational fit vs. CST fit

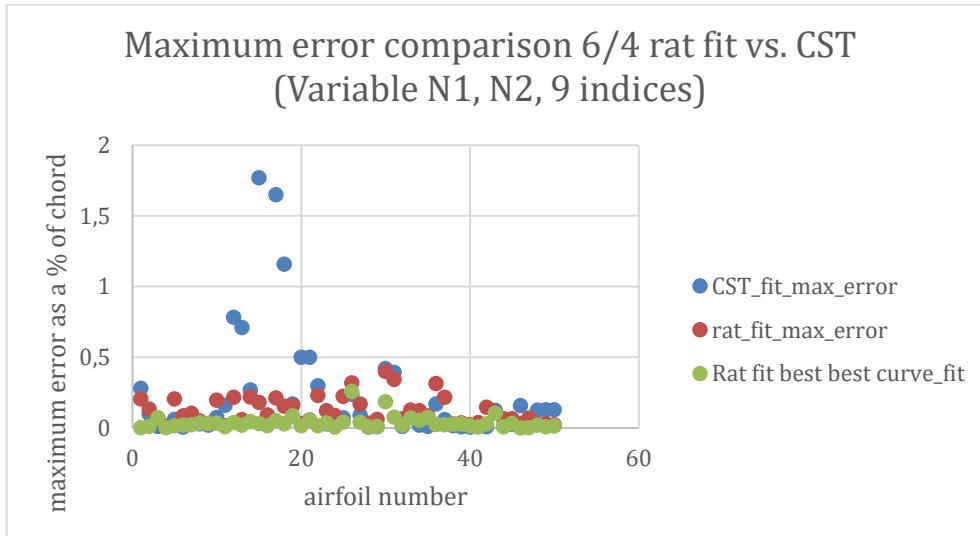


Fig 2. Maximum error comparison for Rational fit vs. CST fit

It is worth taking a further look at the outliers for the CST fit, in both RMS error and maximum error.

As stated above, these will be the airfoils that require the introduction of a trailing edge thickness, as well as a chord angle for the CST evolutionary algorithm. Since it is clear that the rational fit obtained with the `curve_fit` function in Python is much better than the one obtained through the CMA-ES evolutionary algorithm, we shall compare the improved CST fit with it, and not the other rational fit.

After modifying the algorithm to account for these variables, we get the following results:

RMS error comparison improved CST vs rat_fit with curve_fit function

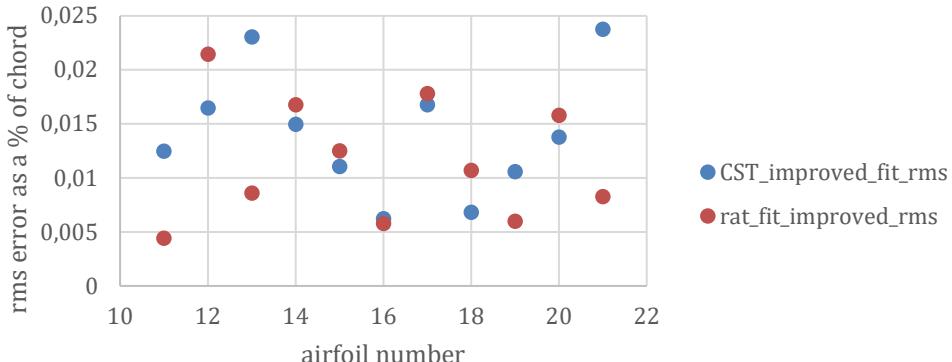


Fig 3. RMS error comparison for improved CST fit vs. Rational fit obtained through the curve_fit function

Maximum error comparison improved CST vs rat_fit with curve_fit function

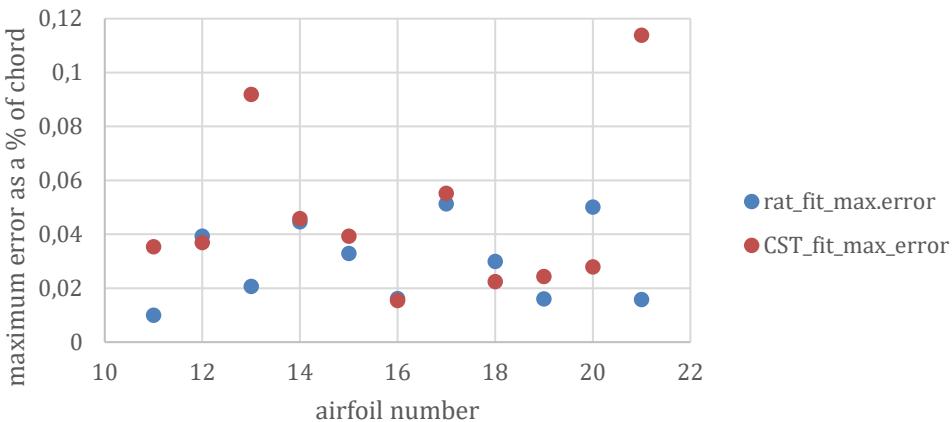


Fig 4. Maximum error comparison for improved CST fit vs. Rational fit obtained through the curve_fit function

We present here an example, as a proof-of concept (for sd7037), for the lower surface: Rational fit (6/4), for a total of 11 parameters:

$$f(x) = \frac{a_0 + a_1x + a_2x^2 + a_3x^3 + a_4x^4 + a_5x^5 + a_6x^6}{1 + b_1x + b_2x^2 + b_3x^3 + b_4x^4}$$

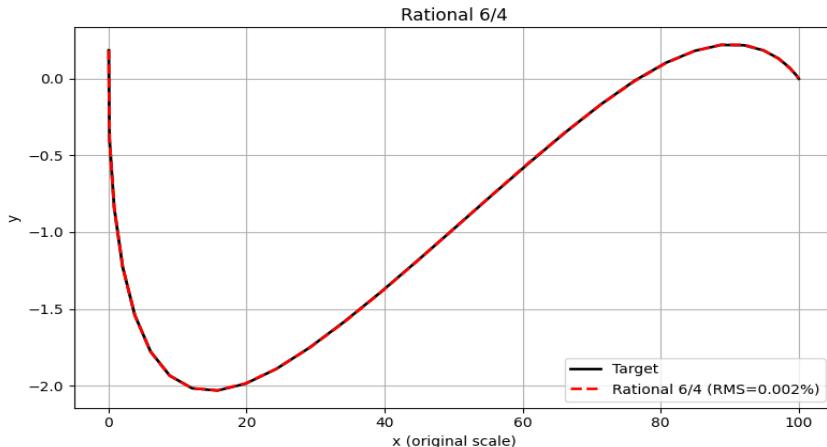


Fig. 5. Rational fit. The numerator of the fraction is a polynomial of degree 6, the denominator is a polynomial of degree 4. Rms_error = 0.00185% of chord; Max_error = 0.00314% of chord

The values of the 11 parameters are:

$a_0=0.0170418694880304$
 $a_1=-49.6688070077132$
 $a_2=-10158.5833249589$
 $a_3=-157200.433447991$
 $a_4=389201.112168681$
 $a_5=-204092.114481554$
 $a_6=-17669.7386052767$
 $b_1=10968.789053471$
 $b_2=647270.779409408$
 $b_3=4308287.49187513$
 $b_4=-3860183.54224129$

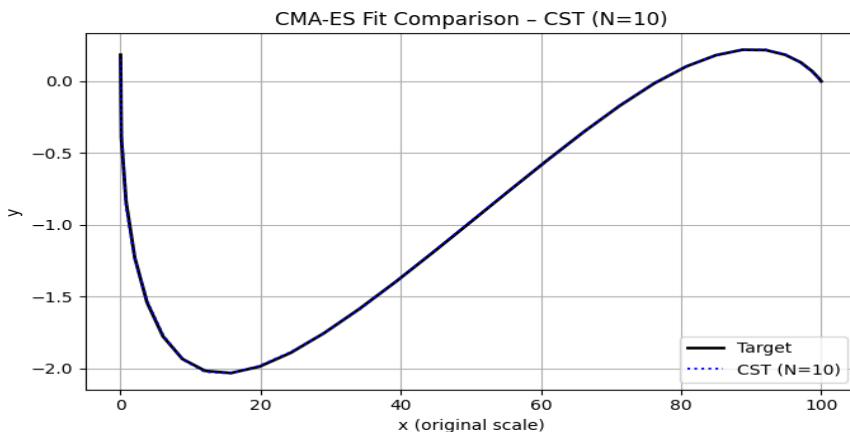


Fig. 6 CST fit (11 indexes, plus variable N1, N2 and trailing edge thickness and chord angle variables). Rms_error = 0.01547%; Max_error = 0.0645%

4. DISCUSSIONS

From the results, we can clearly see that our fit has the potential to be much better than the CST fit, if the evolutionary algorithm is properly optimized. This comes from the fact that the rational fit obtained through the `curve_fit` function gives lower rms and maximum errors than both fits obtained through the evolutionary algorithm. We can also see that even the rational fit obtained through the evolutionary algorithm performs comparable to the CST fit.

These observations also hold up when considering the improved CST fit that takes into account the trailing edge thickness and chord angle. From fig. 3 and fig. 4, we can see that while our fit has similar performance to the CST in terms of the rms errors, it performs consistently better in terms of the maximum error.

5. CONCLUSIONS

Following our data analysis, we can make the following statements:

Our fit can be used to characterise airfoils, especially airfoils where CST might struggle (such as heavily cambered ones) to a very high degree of accuracy

Thus, it can be concluded that our rational fit would be superior for airfoil parametrization in applications where heavily cambered airfoils are generally used and would be worth using over other methods.

REFERENCES

- [1] Kulfan, B. M. (2006). *Universal Parametric Geometry Representation Method*. AIAA Paper 2006-6948.
- [2] V. I. R. Niculescu, D. Popescu, A. G. Popescu, A versatile analytical representation of the different aircraft wings, *INCAS Bulletin*, Volume 16, Issue 3/2024, pp. 61-65, <https://doi.org/10.13111/2066-8201.2024.16.3.6>
- [3] * * * <http://airfoiltools.com/> .
- [4] UNPUBLISHED – Oral Lesson. Granada Seminar on Computational and Statistical Physics 2025 - *A simple analytical representation of aircraft wings: concave - convex case* - Mihnea Butiurca, Valentin Ioan Remus Niculescu, Dumitru Popescu, Stefan Steblea
- [5] N. Hansen and A. Ostermeier, “Completely derandomized self-adaptation in evolution strategies.” *Evolutionary Computation*, 9(2):159–195, 2001.
- [6] N. Hansen, “pymca – A Python implementation of CMA-ES,” <https://github.com/CMA-ES/pymca>.
- [7] * * * List of all airfoils used, and their corresponding numbers.

List of all airfoils used, and their corresponding numbers:

1. sd7037
2. ag35
3. fx60126
4. s6063
5. mh114
6. rg15
7. e205
8. naca643618
9. naca633618
10. naca4415
11. naca23015
12. ls417

- 13. ls413
- 14. sc20414
- 15. sc20712
- 16. s4053
- 17. sc20714
- 18. sc20610
- 19. sc20410
- 20. sg6051
- 21. sg6050
- 22. sg6042
- 23. sg6040
- 24. mh120
- 25. mh112
- 26. du861372
- 27. du84132v
- 28. s2055
- 29. s2048
- 30. s1210
- 31. s1223
- 32. goe703
- 33. fx66s196
- 34. fx79w151a
- 35. e210
- 36. e423
- 37. clark-y
- 38. naca632615
- 39. naca65210
- 40. naca65206
- 41. n64800a
- 42. naca64a010
- 43. naca6412
- 44. naca6409
- 45. naca662415
- 46. naca0015
- 47. naca0009
- 48. naca23012
- 49. naca4412
- 50. naca2412